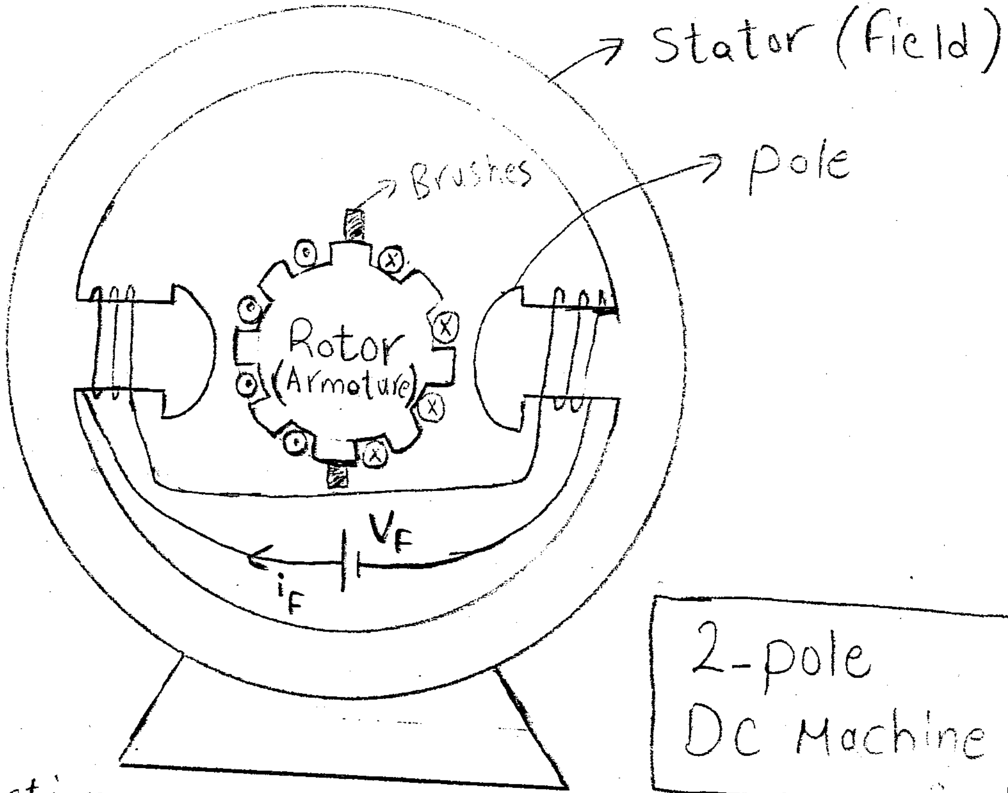
Dc Machines



2-pole
Dc Machine

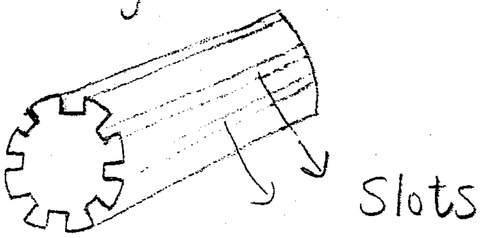
Construction

① Stator

- Carries the field winding (exciter)
- Field winding is Connected to Dc Voltage source
- Field winding produces the magnetic Flux.

② Rotor

- Carries armature winding
- Rotor has a cylindrical shape with slots
- The conductors are placed in these slots.
- e.m.f is induced on the terminals of armature winding.



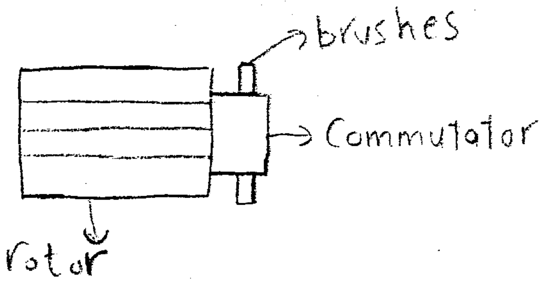
- Rotor is laminated to reduce eddy losses.

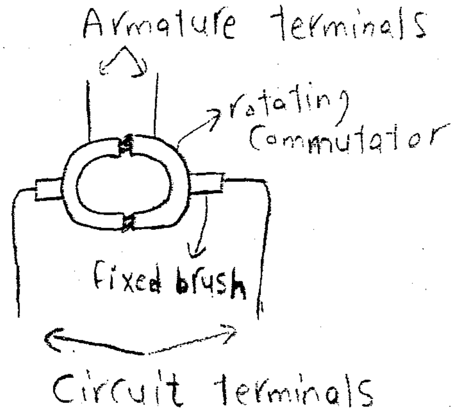
③ Commutator

* It's a copper cylinder divided into isolated segments
* It's connected to armature winding terminals
* It's a rotating part.

(4) Carbon brushes

- They are fixed Contacts
- They are in direct Contact with the Commutator





(5) Air gap:

- It's the Clearance between Stator and rotor

Notes

(a) Commutator is used to

→ Convert Ac Voltage to DC Voltage in Case of DC genartor

→ produce unidirectional torque in DC motor

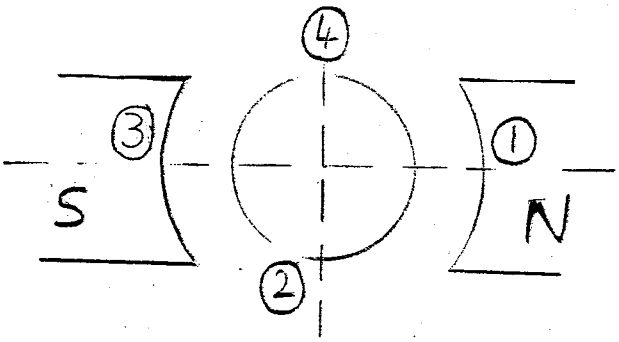
(b) The horizontal axis is Called pole axis,
The Vertical axis is Called interpole axis.

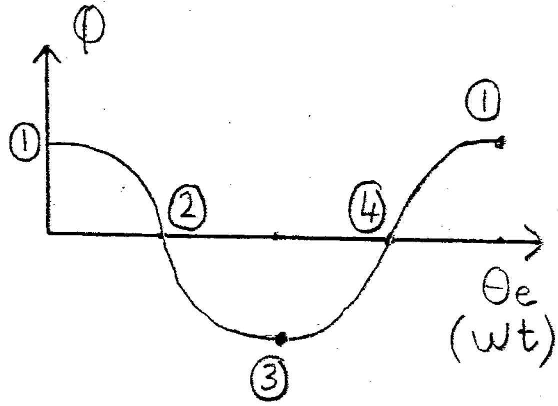
Relation between θ_e, θ_m

$\theta_e = \omega t$; ω is electrical angular frequency

$\theta_m = \omega_m t$; ω_m is mechanical angular frequency

For 2 poles ($P = 1$) no. of pole pairs





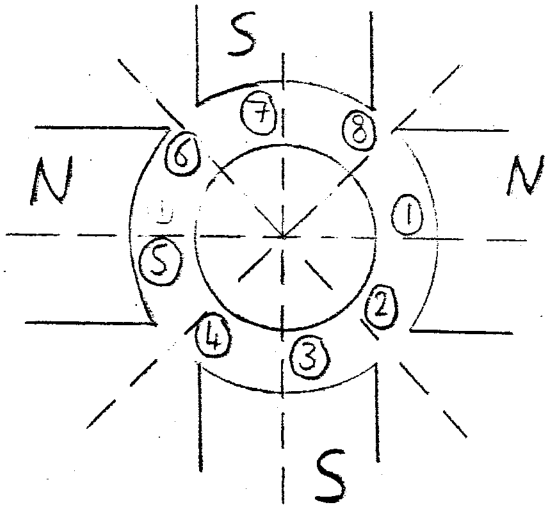
1 → 2 $\theta_m = 90°$ $\theta_e = 90°$

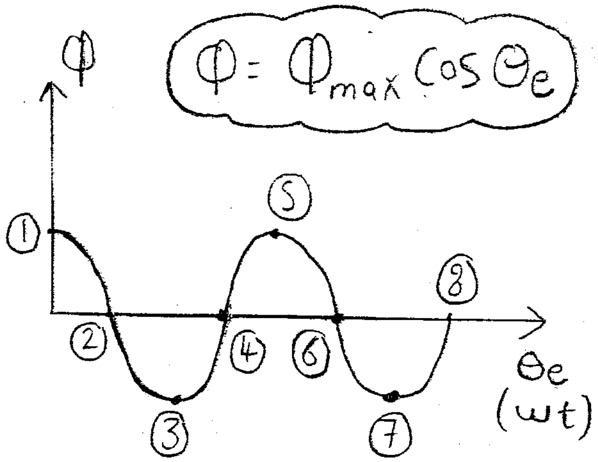
2 → 3 $\theta_m = 90$ $\theta_e = 90$

$\boxed{\therefore \theta_m = \theta_e}$

For 2 poles

For 4 poles $(p=2)$





$1 \rightarrow 2$ $\theta_m = 45$ but $\theta_e = 90$

$2 \rightarrow 3$ $\theta_m = 45$ but $\theta_e = 90$

$\boxed{\therefore \theta_e = 2\theta_m}$

$\therefore$ For (p) poles

$$\theta_e = p * \theta_m$$

$$\therefore \omega_e = p\ \omega_m$$

حفظ

- When $p = 1$ $\Rightarrow$ $\theta_e = \theta_m$, $\omega_e = \omega_m$
- When $p = 2$ $\Rightarrow$ $\theta_e = 2\theta_m$, $\omega_e = 2\omega_m$

Relation between f_e & n_m

$\because \theta_e = p\,\theta_m$

$\therefore \dfrac{d\theta_e}{dt} = p\,\dfrac{d\theta_m}{dt}$

$\omega_e = p\,\omega_m$

$\therefore 2\pi f_e = p * 2\pi f_m$

$\therefore f_e = p f_m$

But $f_m = \dfrac{n}{60}$

where n: Number of revolutions per minute (rpm)

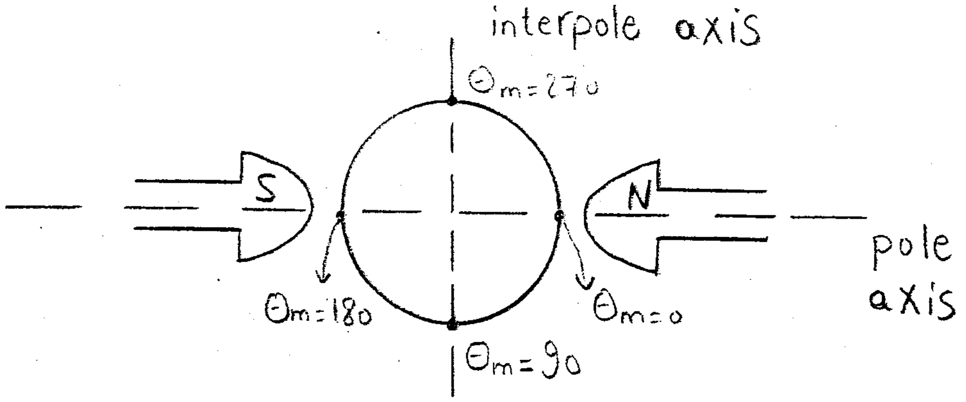
$$\therefore f_e = \frac{pn}{60}$$

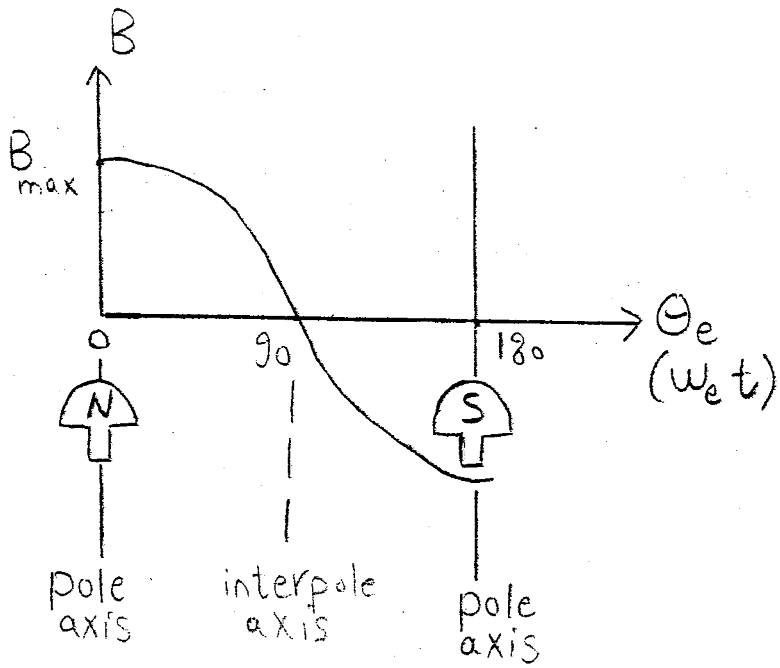
f_e: electrical frequency (HZ)

p: Number of pole pairs

n: Mechanical speed of rotor in rpm

Flux denisty distribution in DC machine [Flux of stator]





$$\therefore B = B_{max} \cos(w_e t)$$

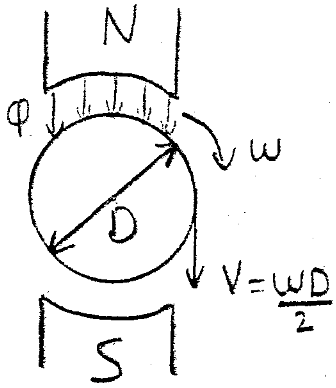
This means that the Flux Varies Sinusoidal

E.M.F equation in DC Machines "proof"

$$e_c = B\,l\,V$$

where

- $e_c \rightarrow$ Induced emf per Conductor
- $B \rightarrow$ Flux denisty $= \dfrac{\Phi}{A}$
- $l \rightarrow$ Conductor length
- $V \rightarrow$ lineor speed
- $\omega \rightarrow$ Angular Speed (ω_m)
- $n \rightarrow$ R.p.m (revolution per minute) $\quad \boxed{\omega = \dfrac{2\pi n}{60}}$
- $D \rightarrow$ Rotor diameter
- $\Phi \rightarrow$ Flux per pole



$$\Rightarrow B = \frac{\Phi}{A} = \frac{\Phi}{\frac{\pi D l}{2}} = \frac{2\Phi}{\pi D l} \quad , \quad V = \frac{\omega D}{2} = \frac{\pi D n}{60}$$

$$\therefore e_c = \frac{2\Phi}{\pi D l} * l * \frac{\pi D n}{60} = \frac{2n\Phi}{60}$$

For Z Conductor $\Rightarrow \boxed{e_Z = e_c * Z}$

where e_Z : Induced emf in all Conductors

$$E_a = \frac{e_z}{a}$$

E_a = Induced emf in the armature

a = Number of parallel paths

$$\therefore E_a = \frac{2n\phi Z}{a * 60} = \frac{2Z}{60a} n\phi$$

For (2p) poles $\Longrightarrow$ $\boxed{E_a = \frac{2PZ}{60a} n\phi}$

$\therefore$ $\boxed{E_a = K n\phi}$ where $K = \frac{2PZ}{60a}$

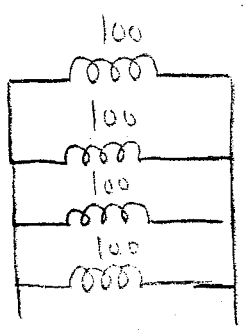
#

What are parallel paths (a) للفهم فقط

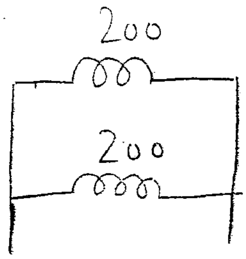
* If $Z = 400$ (total number of conductors = 400)

Not all conductors are connected in series

To reduce voltage drop and losses



$a = 4$



$a = 2$

Dc machine can operate as

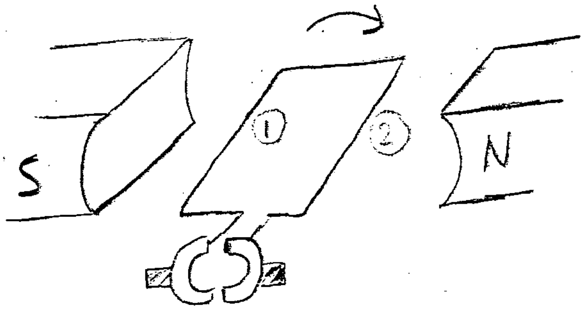
1. Dc generator
2. Dc motor

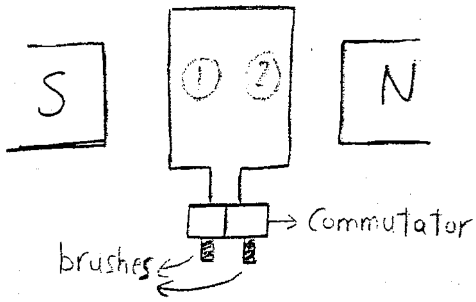
[1] DC generator

Theory of operation

(a) The field current produces flux

(b) If the rotor (armature coil) is externally rotated

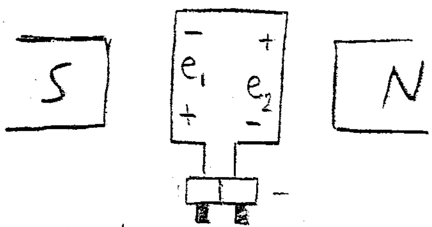




(c) A Voltage will be induced on both Conductors (1,2)

$e_1 = BLV \qquad e_2 = BLV$

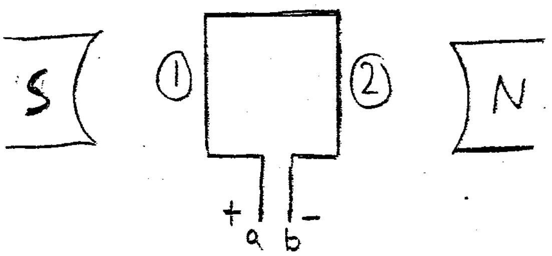
$e_{coil} = 2BLV$



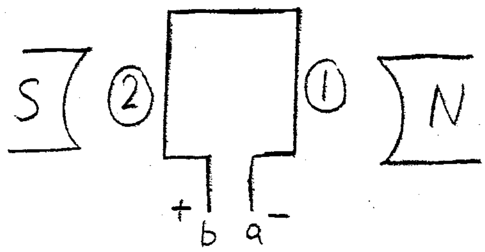
(d) The Commutator Converts Ac Voltage into Dc.

Why do we use Commutator & brushes للفهم فقط

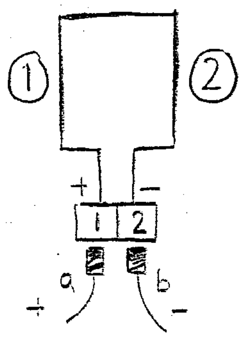
In First half Cycle of the Coil rotation

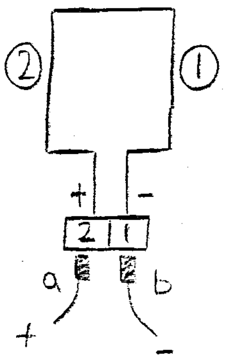


In Second half Cycle of the Coil rotation



The Voltage across the coil changes its polarity, So we use Commutator and brushes as a mechanical rectification to get DC Voltage from the Coil

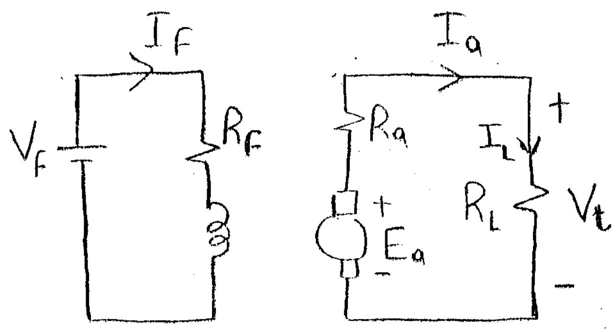




* brush (a) is +ve in both half cycles
  brush (b) is -ve " " " "

Types of DC generators

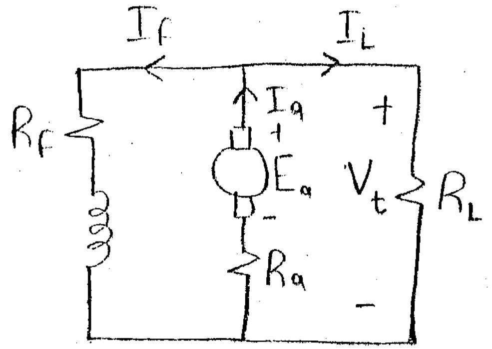
I Separately excited



$$V_f = I_f R_f$$

$$E_a = V_t + I_a R_a$$

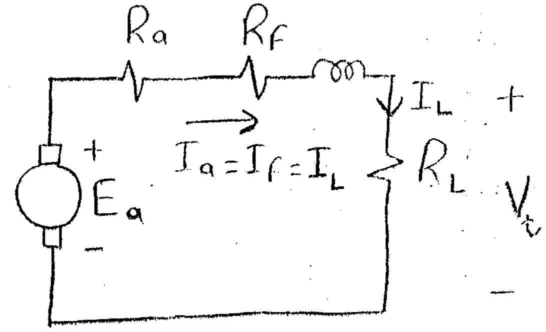
II Shunt



$$I_f = \frac{V_t}{R_f}$$

$$E_a = V_t + I_a R_a$$

III Series

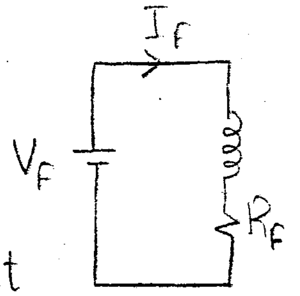


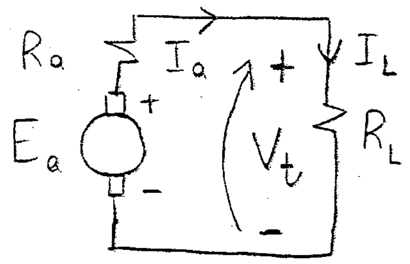
$$E_a = V_t + I_a (R_a + R_f)$$

$$I_a = I_L = I_f$$

I Separately excited DC generator

⇒ Field circuit





$V_f = I_f R_f$

* I_f → field current
* R_f → field resistance

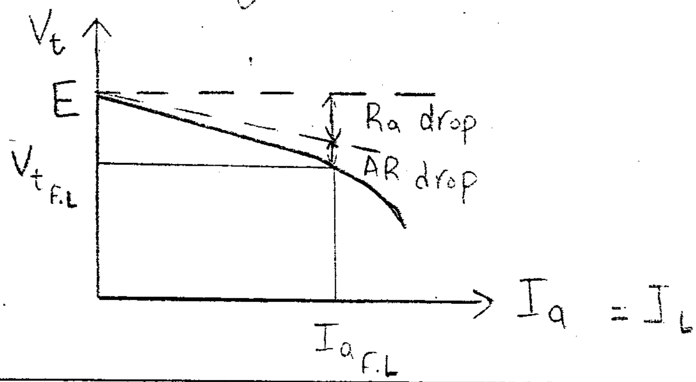
⇒ Armature circuit

$E_a = V_t + I_a R_a +$ (Armature reaction drop)

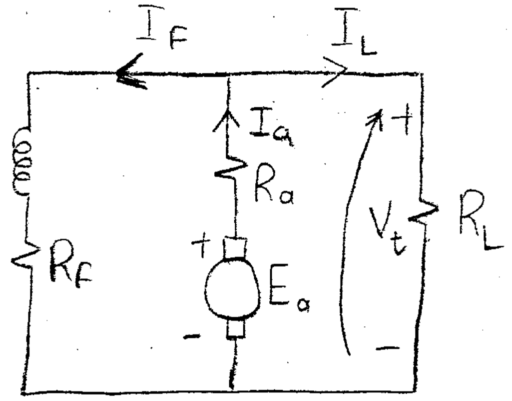
* R_a → Armature resistance
* I_a → Armature current
* V_t → Terminal Voltage

If (AR) is neglected ⇒ $E_a = V_t + I_a R_a$

⇒ External characteristic of separately excited DC generator



II Shunt DC generator



$$I_f = \frac{V_t}{R_F}$$

$$E_a = V_t + I_a R_a$$

The Voltage drop is due to

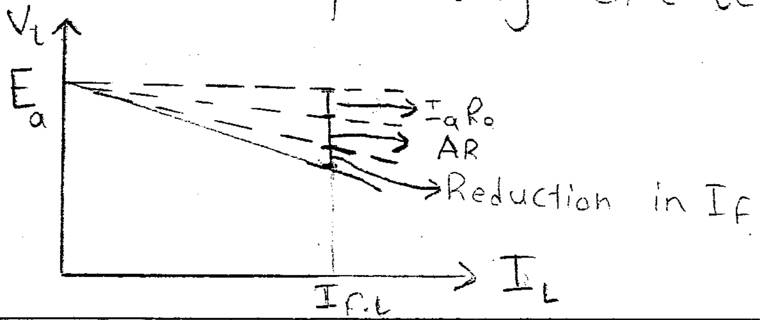
1. R_a drop
2. Armature reaction drop
3. Decrease in field current

as $I_f = \frac{V_t \downarrow}{R_F}$ (V_t decrease as I_L increases)

$\therefore I_f \downarrow \rightarrow \Phi \downarrow \rightarrow (E_a = Kn\Phi) \downarrow \rightarrow V_t \downarrow$

that's why shunt DC generator has external C/C's which is more drooping than that of separately excited (عشان sep. excited بيجيله اول نوعين من ال drop فقط)

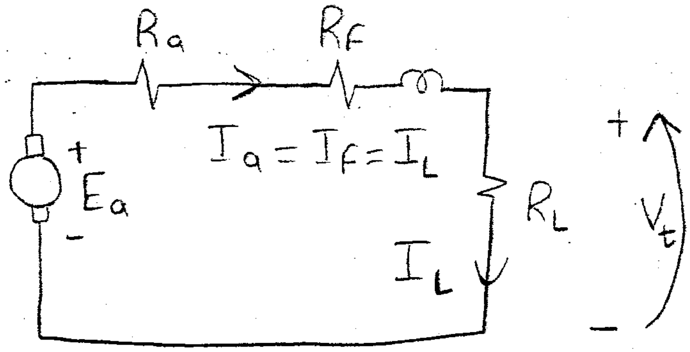
External C/C's



III Series DC generator

$I_a = I_f = I_L$

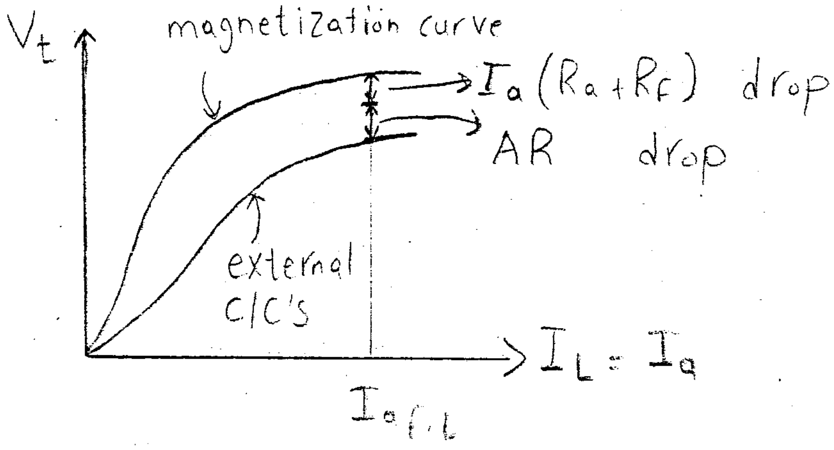
$E_a = V_t + I_a(R_a + R_f)$



The Voltage drop is due to

1. $(I_a R_a + I_a R_f)$ drop
2. AR drop

External C/C's

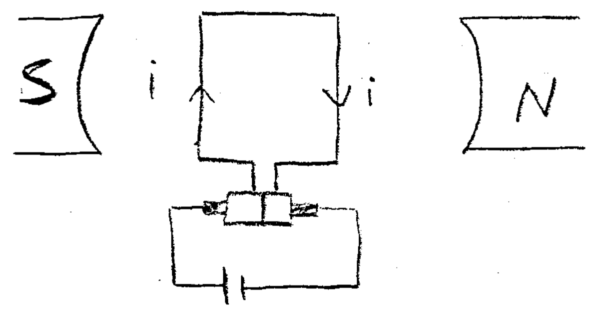


② Dc motor

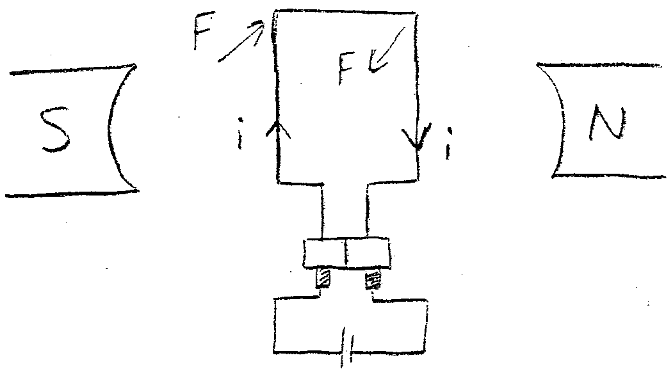
Theory of operation

ⓐ The Field Current produces Flux

ⓑ IF the armature winding terminals are Connected to an external DC Source, then a Current will Flow in armature winding.



ⓒ Now both Conductors (1,2) has a current i and placed in a magnetic field (B), So A Force will be produced on both Conductors but in opposite direction. ($F = BIL$)



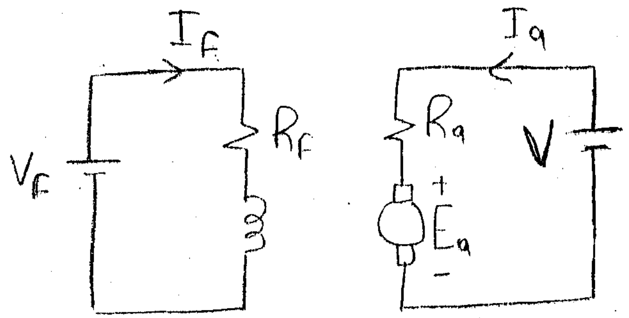
ⓓ So, the Coil starts to rotate with a torque $T = BILW$

ⓔ As the Coil rotates in a magnetic field, so a back emf will be induced on the Coil (as in generator)

ⓕ The Commutator converts the torque into unidirectional torque

Types of Dc motors

I Separately excited



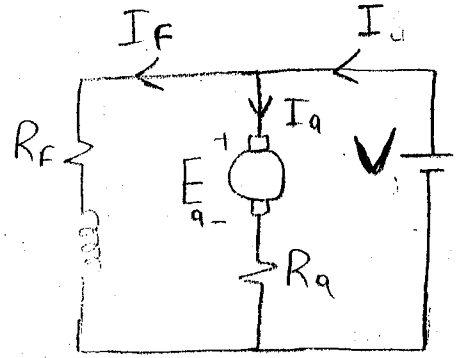
$V_f = I_f R_f$

$E_a = V - I_a R_a$

$E_a = K n \phi \Rightarrow E_a \propto n I_f$

$T = K I_a \phi \Rightarrow T \propto I_a I_f$

II Shunt



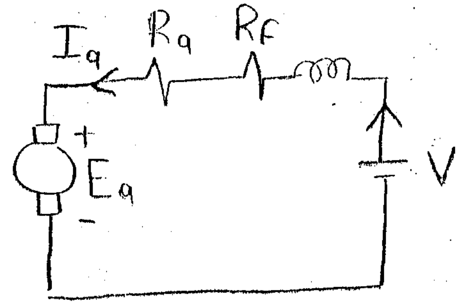
$I_f = \dfrac{V}{R_f}$

$E_a = V - I_a R_a$

$E_a = K n \phi \Rightarrow E_a \propto n I_f$

$T = K I_a \phi \Rightarrow T \propto I_a I_f$

III Series



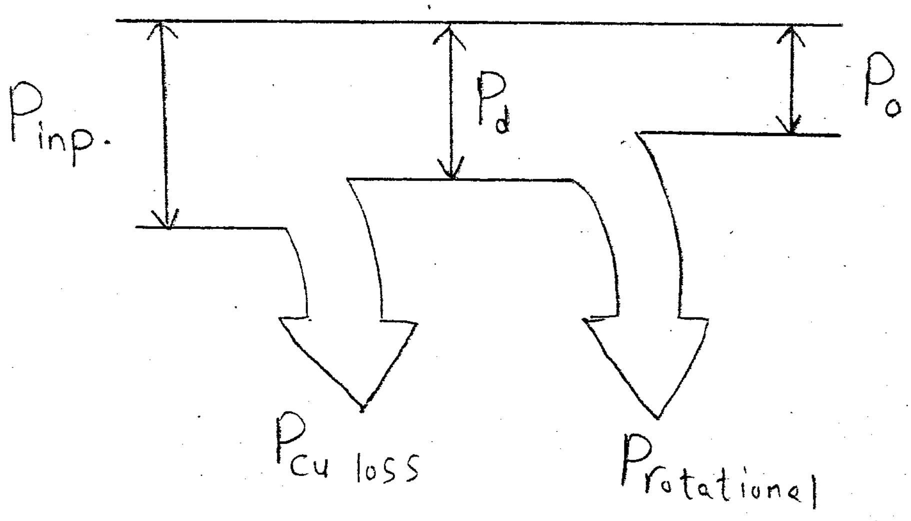
$E_a = V - I_a (R_a + R_f)$

$E_a = K n \phi \Rightarrow E_a \propto n I_a$

$E_a \propto n I_f$

$T = K \phi I_a \Rightarrow T \propto I_a^2$

power flow in DC motor



* $P_{inp} \equiv$ input power $= V_s I_{inp.}$ → input current

* $P_{Cu_{loss}} = I^2 R$ (depends on connection)

* $P_d \equiv$ developed power $= E_a I_a = T_d \omega_m$

* $P_r \equiv$ rotational loss

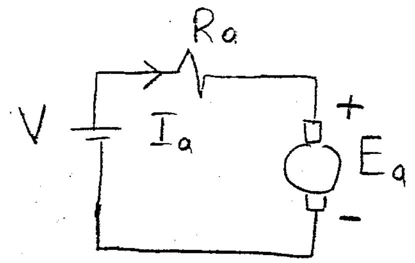
* $P_o \equiv$ output power $= T_{sh} * \omega_m$ (T_{sh} ↳ Shaft torque)

$$\eta = \frac{P_o}{P_{inp.}} = \frac{P_{inp} - \sum losses}{P_{in}}$$

* $P_o = P_d - P_{rotational}$ * $P_d = P_{in} - P_{Cu\ loss}$

Role of back emf (E_a) in motors

E_a produces a current opposite to the supply current, so the armature current is limited within acceptable range



Starting of DC motors

$\because V = E_a + I_a R_a$

$\therefore I_a = \dfrac{V - E_a}{R_a}$ but $E_a = K n \phi$

But at starting $(n=0) \Rightarrow E_a = 0$

$\therefore I_a|_{st.} = \dfrac{V-0}{R_a} \uparrow\uparrow$ (very high)

$\therefore$ The armature current is very high at starting; so we must use starters (starting resistors to reduce $I_a|_{st.}$)

Sheet 3 - Continued

[11] page(13)

[12]

(i) page(7,8)

(ii) page(19)

(iii) page(17)

[13] * Different methods of excitation

→ Separately excited generators

→ Self excited generators

→ Series

→ Shunt

* Characteristics → page(11)

* Significance of back emf → page(19)

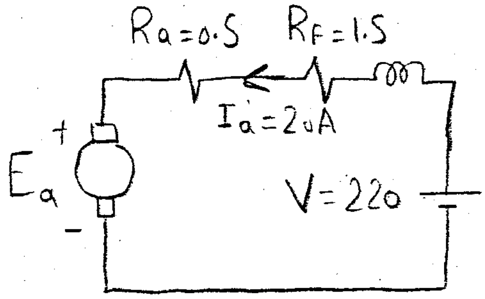
[17] The armature of DC machine is laminated to reduce eddy current loss

(14) Series motor

- $R_a = 0.5\,\Omega$, $R_f = 1.5\,\Omega$
- $I_a = 20A$ when $n = 1200rpm$
- $V = 220V$, $P_{rotational} = 150W$

Find P_o, η

Solution



$E_a = V - I_a(R_a + R_f)$

$E_a = 220 - 20(0.5 + 1.5)$

$\therefore E_a = 180V$

$\Longrightarrow P_o = P_d - P_{rot.}$; $P_d = E_a I_a = 3600W$

$\therefore P_o = 3600 - 150$

$P_o = 3450W$

$\Longrightarrow P_i = V * I_a = 4400$

$\Longrightarrow \eta = \frac{P_o}{P_i} = \frac{3450}{4400} = 78.4\%$

$\eta = 78.4\%$

15 . DC motor (Assume Separately excited)

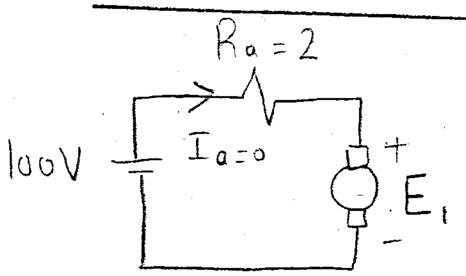
- **at No load** · $V = 100V$, $n = 1200 rpm$
- $R_a = 2\Omega$
- **Find** T, I_a if $V = 220V$, $n = 1500 rpm$
- I_f is constant

Solution

Case (1) $V = 100V$

$n_1 = 1200 rpm$

No load ($I_a = 0$)



$\boxed{E_1 = 100V}$

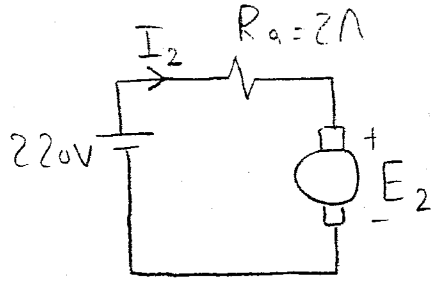
$E_1 = Kn\Phi = K'n$

$100 = K' * 1200$

$\boxed{K' = 0.083}$

Case (2) $V = 220V$

$n_2 = 1500 rpm$



$\Rightarrow \frac{E_2}{E_1} = \frac{n_2}{n_1}$

$\frac{E_2}{100} = \frac{1500}{1200} \Rightarrow \boxed{E_2 = 125V}$

$\Rightarrow$ But $E_2 = 220 - I_2 * 2$

$\therefore I_2 = 47.5A$

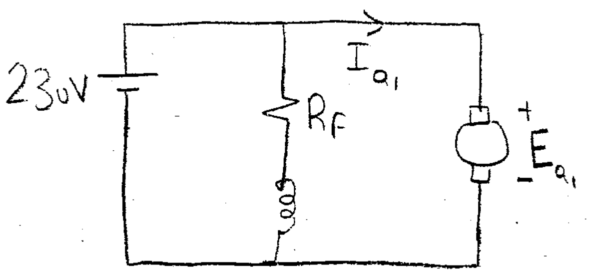
$T = KI_a\Phi = K'I_a = 3.96 N.m$

(16). DC Shunt motor

- Constant field (I_F = Const.)
- $T \propto n$
- $I_a = 30A$ when $n_1 = 750$ rpm
- $R_{series} = 10\,\Omega \Longrightarrow n_2 = ??$
- R_a is neglected

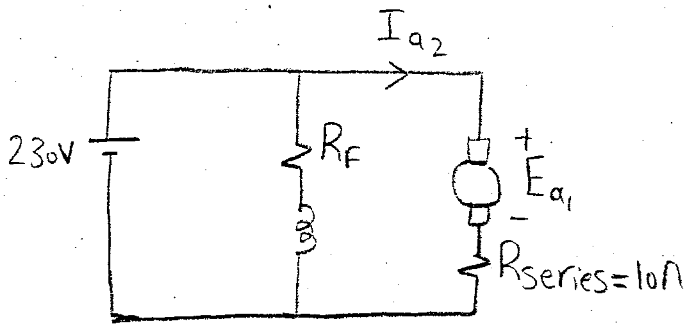
Solution

Case (1) $n_1 = 750$ rpm, $I_{a_1} = 30A$



$E_{a_1} = 230V$

Case (2) $R_{series} = 10\,\Omega$



$E_{a_2} = 230 - 10\, I_{a_2}$

$\Longrightarrow$ But $E \propto n \overset{\text{Constant}}{\phi} \Longrightarrow E \propto n$

$$\therefore \frac{E_2}{E_1} = \frac{n_2}{n_1}$$

$$\frac{230 - 10 I_2}{230} = \frac{n_2}{750}$$

$$0.306\,N_2 + 10\,I_2 = 230 \quad \rightarrow \text{(1)}$$

$\Rightarrow$ But $T \propto n$ (given)

$$T \propto \underbrace{\phi}_{\text{const.}} I_a \Rightarrow T \propto I_a$$

$$\therefore \frac{T_2}{T_1} = \frac{n_2}{n_1} = \frac{I_2}{I_1}$$

$$\therefore \frac{n_2}{750} = \frac{I_2}{30}$$

$$\therefore n_2 = 25\,I_2 \quad \rightarrow \text{(2)}$$

Solving (1), (2) we get

$$I_{a_2} = 13\text{ A}$$

$$n_2 = 325.7 \text{ rpm}$$